

## TOPEX/POSEIDON OPERATIONAL ORBIT DETERMINATION RESULTS USING GLOBAL POSITIONING SATELLITES

Joseph R. Quinn<sup>\*</sup> and Peter J. Wolff<sup>†</sup>

Results of operational orbit determination, performed as part of the TOPEX/Poseidon (T/P) Global Positioning Satellite (GPS) demonstration experiment, are presented in this paper. Elements of this experiment include the GPS satellite constellation, GPS Demonstration Receiver on-board T/P, six ground GPS receivers, the GPS Data Handling Facility and the GPS Data Processing Facility (GDPF). Carrier phase and P-code pseudo range measurements from up to 25 GPS satellites to the seven GPS receivers are processed simultaneously with the GDPF software MIRAGE to produce orbit solutions of T/P and the GPS satellites. Daily solutions yield sub-decimeter radial accuracies compared to other GPS, LASER and DORIS precision orbit solutions.

### INTRODUCTION

The Global Positioning Satellite (GPS) Data Processing Facility (GDPF) was developed to demonstrate operational orbit determination and navigation support for TOPEX/Poseidon. Orbit solutions are based on data collected by the GPS Demonstration Receiver (GPSDR), on-board TOPEX/Poseidon, and six ground stations. In addition, the GDPF is intended to evolve into a NASA resource for future low Earth orbiting missions under the Office of Space Communications.

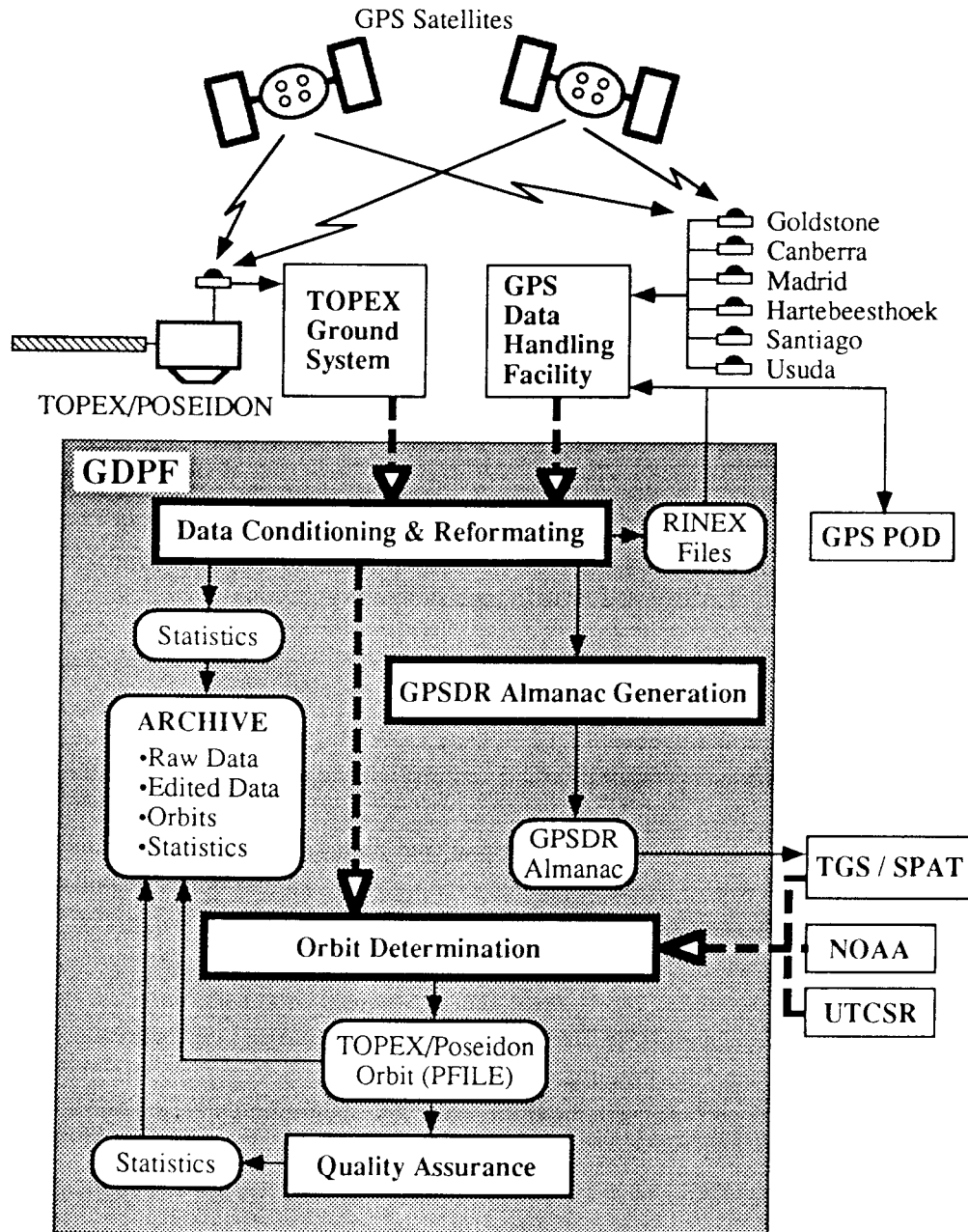
An updated software set, based on the JPL institutional Orbit Determination Program (ODP), was created and named "MIRAGE." It stands for: Multiple Interferometric Ranging Analysis using GPS Ensemble. MIRAGE maintains the complete interplanetary capability of the ODP software with the additional multi-satellite and precision modelling

---

\* Member of Technical Staff, Jet Propulsion Laboratory, California Institute of Technology, MS 301-125J, 4800 Oak Grove Drive, Pasadena, California 91109. Member AIAA.

† Member of Technical Staff, Jet Propulsion Laboratory, California Institute of Technology, 4800 Oak Grove Drive, Pasadena, California 91109.

**Figure 1. - GPS Data Processing Facility Interfaces**



features required for sub-decimeter orbit determination. The scope of the GDPF includes: pre-processing observations, performing orbit determination, producing predicted GPS and TOPEX/Poseidon satellite almanacs for mission operations, and archiving raw and processed data. Figure 1. shows the interfaces of the GDPF.

## **OBSERVATION PRE-PROCESSING**

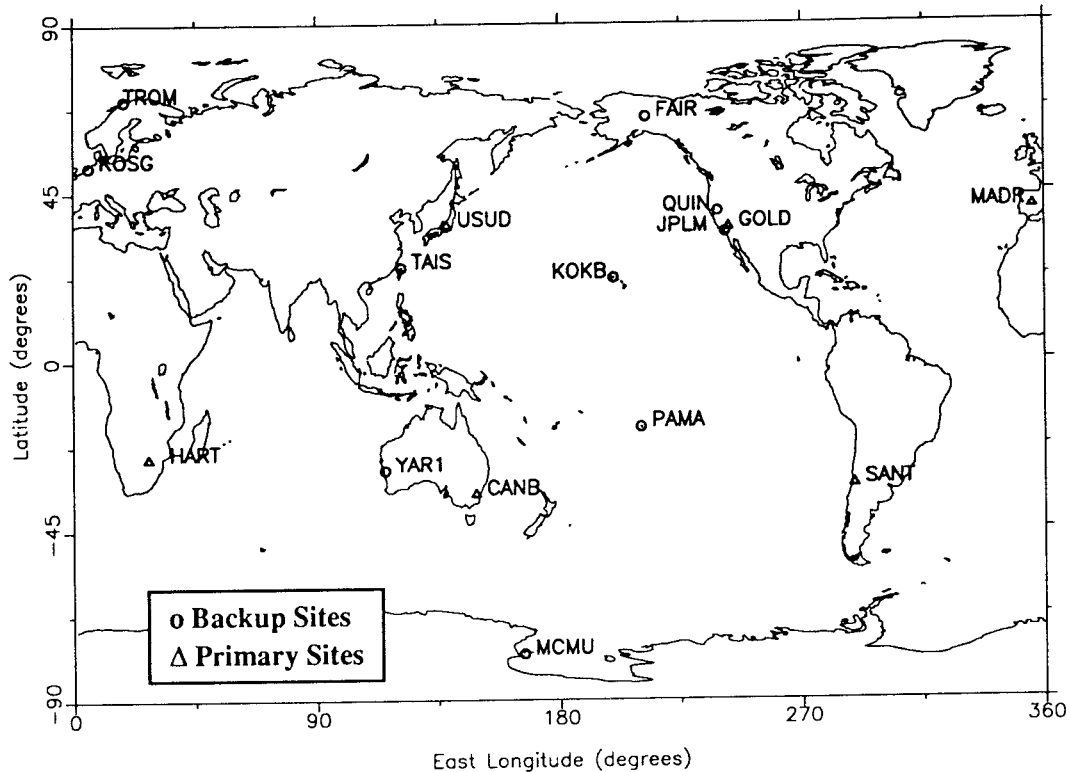
Daily TOPEX flight receiver raw data are collected from the TOPEX Ground System within 24 hours of the last observation. The raw data consists of carrier phase every second and P-Code pseudorange every 10 seconds. In addition, the GPSDR on-board navigation solution (i.e., clock, position and velocity) are provided every 10 seconds.

Automated reformatting and outlier and cycle slip editing is performed first. Next, the data are decimated to five minute intervals and a time tag correction, based on a linear fit to the navigation clock solution, is applied. Finally, linear combinations of the pseudorange ( $P_1$  and  $P_2$ ) and carrier phase ( $L_1$  and  $L_2$ ) dual frequency measurements are computed to produce ionosphere calibrations. These are applied to the raw  $P_1$  and  $L_1$  observations to produce the orbit determination observables  $P_C$  and  $L_C$ .

The ground GPS receiver observations are available from the GPS Data Handling Facility about 36 hours after the last data were collected. Both the carrier phase and pseudorange are provided in RINEX<sup>1</sup> format at 30 second samples. The same editing and calibration steps are performed as described above for the GPSDR. In addition to the six core ground sites, data from nine backup sites are also collected and processed. The primary and backup ground station locations are shown in Figure 2.

For MIRAGE orbit determination processing, a merged file of edited GPSDR and ground receiver data is created in standard MIRAGE format. Two additional text files, in RINEX format, are produced for export. One is the raw GPSDR data while the other is the edited, calibrated and compressed GPSDR measurements. All files are archived along with data collection and pre-processing statistics.

**Figure 2. - TOPEX/GPS Ground Station Network**



## ORBIT DETERMINATION STRATEGY

Thirty hour data sets are constructed from the pre-processed observations to produce a 24 hour orbit solution. The additional data is fit to allow for internal consistency checks of the daily overlaps. Global GPS constellation coverage is realized by selecting a minimum of six ground station GPS receiver sites. Additional sites are selected to fill gaps during primary site outages.

Orbit determination using MIRAGE consists of three major steps. Iteration through each step is performed until convergence of the state solutions and observation residuals is achieved. The three steps are:

- Trajectory Propagation
- Observation Processing
- Filtering and Smoothing

**Trajectory Propagation** - To achieve sub-decimeter accuracies several dynamic force models are required. Tables 1 and 2. summarize the force models used in the numerical integration of the TOPEX/Poseidon and GPS satellite trajectories. Reference frame, force, and measurement model parameters are based on TOPEX/Poseidon and International Earth Rotation Service (IERS) standards<sup>2-3</sup>.

**Table 1. - Force Models for TOPEX/Poseidon**

<b><u>Model:</u></b>	<b><u>Description:</u></b>
N-Body:	All Planets, Sun, Moon
Earth Geopotential:	50x50 truncated JGM-2
Indirect Earth-Moon Oblateness:	2x2 Lunar Model
Solid Earth Tides:	IERS
Ocean Tides:	JGM-2
Rotational Deformation:	IERS
Relativity:	Point Mass Earth + Lense-Thirring
Solar Radiation Pressure:	Conical Shadow Model
Atmospheric Drag:	DTM Model
Albedo and Infrared Earth Radiation:	2nd Degree Zonal Model
Empirical Accelerations:	Once/Rev and Twice/Rev Models

**Table 2. - Dynamic Force Models for GPS Satellites**

<b><u>Model:</u></b>	<b><u>Description:</u></b>
N-Body:	All Planets, Sun, Moon
Earth Geopotential:	12x12 truncated JGM-2
Indirect Earth-Moon Oblateness:	2x2 Lunar Model
Solid Earth Tides:	IERS
Ocean Tides:	JGM-2
Rotational Deformation:	IERS
Relativity:	Point Mass Earth + Lense-Thirring
Solar Radiation Pressure:	Rock4 and Rock42 Models

**Observation Processing** - Both carrier phase and P-Code pseudo-range are processed. Table 3. lists the measurement models used for producing observation residuals. Again, these models are adopted based largely on IERS standards.

**Table 3. - Measurement Models**

<b><u>Model:</u></b>	<b><u>Description:</u></b>
Solid Earth Tides:	0th, 1st and 2nd Order Corrections
Rotational Deformation (Pole Tide):	IERS
Ocean Loading:	IERS
Polar Motion:	UTCSR‡
Plate Motion:	Linear Velocities <sup>4</sup>
Earth Center of Mass Offset:	Currently Zero

***Filtering and Smoothing*** - The filter and smoother generate corrections to the parameters affecting the trajectory propagation and the observation processing. MIRAGE employs a numerically stable square root information filter which has the capability to compute the smoothed estimates of time varying stochastic parameters. Our orbit determination strategy employed a fiducial concept where three ground receivers which were assumed to have well known coordinates are held fixed while the filter estimates the positions of three non-fiducial ground stations in addition to the states of the GPS satellites and TOPEX/Poseidon. The filtering strategy consisted of a two stage process – dynamic tracking followed by reduced dynamic tracking. In dynamic tracking the accuracy of the orbit is limited by the precision of the dynamic models applied during trajectory propagation. In reduced dynamic tracking, the high quality geometric information provided by the GPS measurement system is utilized to obtain a high precision TOPEX/Poseidon trajectory. Essentially, reduced dynamic tracking exploits the extreme precision of carrier phase tracking by using it to smooth the geometric solutions obtained from the less precise pseudo-range measurements. Although the success of the reduced dynamic technique is contingent on high precision modeling of the GPS observations, the accuracy of the resultant trajectories are not degraded by deficiencies in the a priori dynamical models.

**Data Weighting** - The measurement precision expected from the GPSDR and ground station observations was determined from ground test prior to launch. Data weights consistent with these analyses are applied during filtering are shown in Table 4.

**Table 4. - GPS Observation Weights**

<b><u>Data Type</u></b>	<b><u>GPSDR</u></b>	<b><u>Ground Station</u></b>
Carrier Phase	2 cm	1 cm
Pseudo-Range	2 m	1 m

---

‡Daily rapid service solutions from University of Texas

Stochastic Clock Estimation - To eliminate synchronization errors due to unstable oscillators, clock biases at the receivers and GPS transmitters are estimated at each measurement time. In the filter, one ground clock is chosen as a reference and a stochastic clock bias is estimated at each of the other receivers and GPS transmitters. A white noise stochastic process is employed with a batch length coinciding with the measurement intervals and the estimated smoothed clock biases are fed back to the observation processing module. As with standard double differencing techniques, the stochastic clock estimation strategy eliminates common clock errors but the stochastic method avoids both the difficulties of selecting a set of non-redundant double difference combinations and the data noise correlations inherent in differenced measurements.

Stochastic Phase Bias Estimation - Continuously tracked GPS carrier phase precisely measures the relative range change between a GPS transmitter and its receiver. However, the carrier phase is ambiguous which necessitates the estimation of a constant phase bias for each continuous pass between a transmitter and a receiver. In the filter, each phase bias is estimated as a white noise stochastic parameter which remains constant over a pass. At tracking discontinuities, the filter applies a white noise stochastic update for the bias parameter corresponding to an individual transmitter/receiver pair. The smoother generates a time profile of phase bias corrections which are applied during subsequent observation processing. This stochastic phase bias estimation strategy is efficient in terms of computation time and memory requirements but it does not attempt to resolve the integer nature of the phase biases.

Stochastic Estimation of Tropospheric Fluctuations - The model for troposphere delay is decomposed into a wet and dry component.

$$\rho = \rho_d R_d(\theta) + \rho_w R_w(\theta)$$

where  $\rho_z$  is the zenith delay and  $R$  is a mapping function which maps the zenith delay to the line of site at elevation  $\theta$ . The fluctuations in the wet zenith delay were modeled as a stochastic random walk. The wet zenith delay was estimated at 5 minute intervals (coincident with the measurement interval) using an a priori sigma of 5 cm and an effective batch-to-batch sigma of 3 mm for the noise driving the random walk process. As with the phase and clock biases, the smoothed time profile of the stochastic fluctuations were fed back into the observation processing module on subsequent iterations of the orbit determination program.

Reduced Dynamic Tracking - The MIRAGE filter executes the reduced dynamic tracking strategy by modeling the three-dimensional accelerations on TOPEX/Poseidon as exponentially time correlated stochastic processes. The relative weighting of the dynamics and geometry may be adjusted by varying the time constant and the magnitude of the process noise uncertainty. A large time constant corresponds to a dynamic strategy while a short time constant emphasizes the geometry. In the orbit determination for TOPEX/Poseidon the three accelerations were updated at five minute intervals; the time constant was 15 minutes with a corresponding batch-to-batch sigma of  $7 \times 10^{-9} \text{ m/s}^2$  for the radial acceleration and  $14 \times 10^{-9} \text{ m/s}^2$  for the spacecraft X and Y accelerations. This choice of filter parameters allowed deficiencies in the non-gravitational force models to be compensated by the stochastic accelerations; however, enough dynamical information is retained so that temporary degradation of the viewing geometry would not seriously reduce the accuracy of the output trajectory<sup>5-7</sup>.

**Table 5. - Estimated Parameters**

<b><u>Parameter(s)</u></b>	<b><u>Number of Parameters</u></b>
TOPEX State	6
GPS States (20 Satellites Average)	120
Station Locations (3 Stations)	9
GPS Solar Pressure Scale Factors and Y-Bias	60
Empirical Dynamic	9
Stochastics: (30 hour arcs with 5 minute updates)	
Troposphere	6
TOPEX and Ground Clocks (1 master clock fixed)	26
Carrier Phase Biases	~130
Accelerations (X,Y,Z)	3
<hr/>	
TOTAL	~369

## **ORBIT DETERMINATION ACCURACY**

Before launch, the MIRAGE software was inter-compared with the GEODYN and UTOPIA software sets from the Goddard Space Flight Center (GSFC) and the University of Texas Center for Space Research (UTCSR) respectively. The inter-comparison validated all dynamic trajectory models for TOPEX/Poseidon and verified the laser range measurement models. For all cases, including the combined models case, the maximum radial differences were about one centimeter or less for a 10-day orbit.



An additional inter-comparison with the UTCSR GPS software MSODP to validate trajectory models for the GPS satellites was performed. All but the occulting solar radiation pressure produced sub-centimeter, 10-day orbit comparisons. The solar radiation pressure inter-comparison tests have been postponed due to the expected release of improved models.

After launch, the operational orbit determination accuracies have steadily improved as the procedures and techniques have been fine tuned. Accuracy comparisons are broken into three distinct processing phases. The dates and groundtrack repeat cycles for each are:

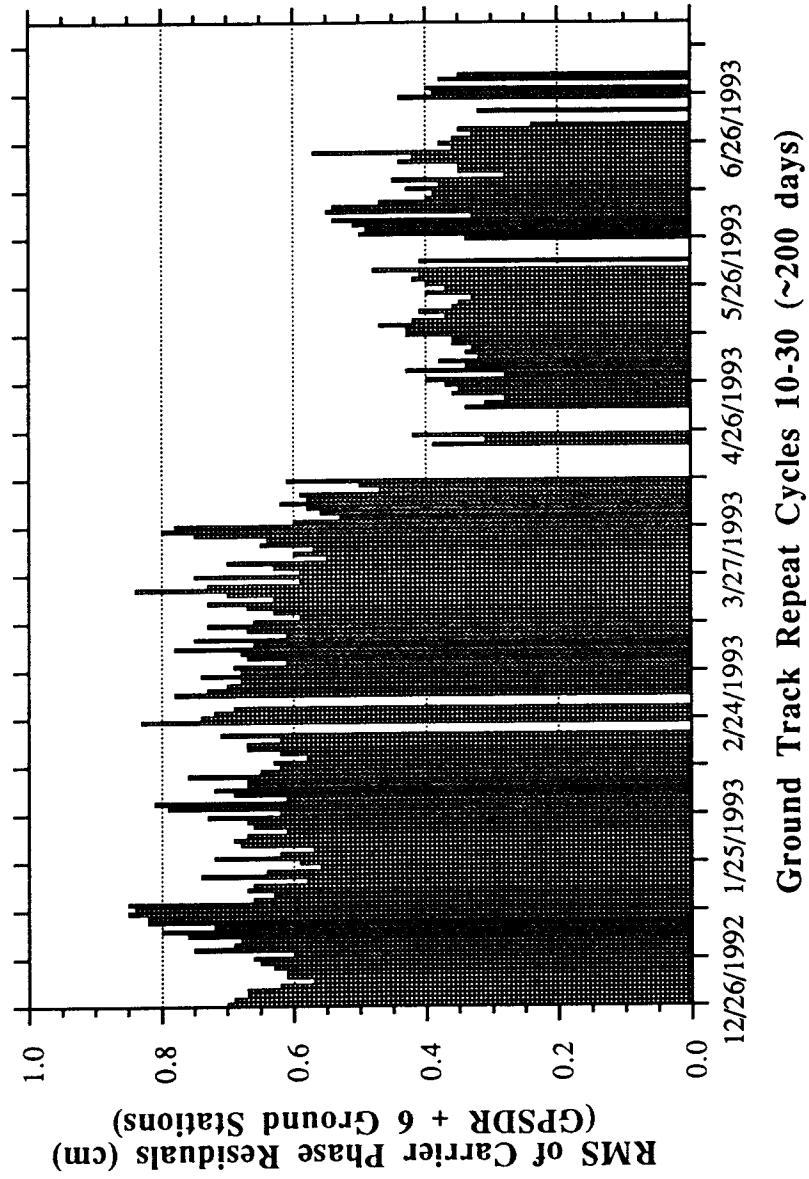
<u>PHASE</u>	<u>DATES</u>	<u>CYCLES</u>
1	November 3, 1992 - December 21, 1992	5-9
2	December 22, 1992 - May 2, 1993	10-23
3	May 3, 1993 - July 16, 1993	24-30

Data prior to cycle five were not considered for this analysis due to difficulties in the early days of the GPSDR plus the occurrence of several anti-spoofing days. Phase 1 processing was performed before many of the internal and external consistency checks (see below) were used; thus, is not representative of the achievable accuracies. Phase 2 processing used 24 hour arcs with the 'dynamic' technique augmented with empirical once and twice per revolution parameters. Phase 3 consists of 30 hour arcs with the additional 'reduced dynamic' tracking strategy.

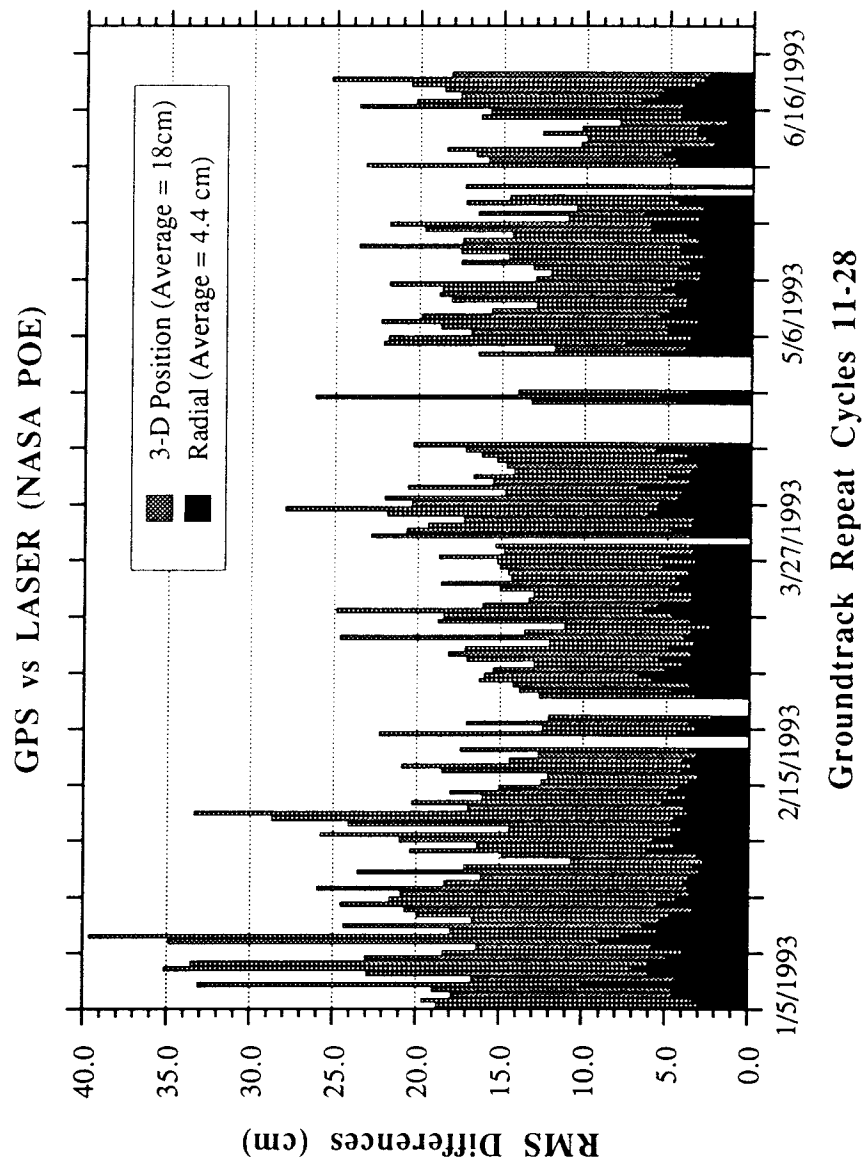
Statistics collected for the GPS carrier phase residuals (observations minus computed values) are presented in Figure 3. These residuals are from Phase 2 and 3 only. A marked reduction in the residuals is seen when the 'reduced dynamic' technique is employed. All gaps are due to GPS constellation anti-spoofing activity when no GPSDR data were available.

TOPEX/Poseidon orbit comparisons have displayed sub-decimeter agreements in the radial component with one day GPS Precision Orbit Determination (POD) solutions and orbits derived from Laser and DORIS data. Figures 4 and 5. show the three dimensional and radial RMS orbit differences during phases 2 and 3. The MIRAGE 'dynamic' solutions are compared with another 'dynamic' solution determined from laser data. The laser solution is an approximately 10 day fit from GSFC's GEODYN program. The basis for the comparisons in Figure 5 are the MIRAGE 'reduced dynamic' solutions. They are compared with another reduced dynamic solution from the GPS GIPSY-OASIS software that is part of the GPS Demonstration Experiment POD segment.

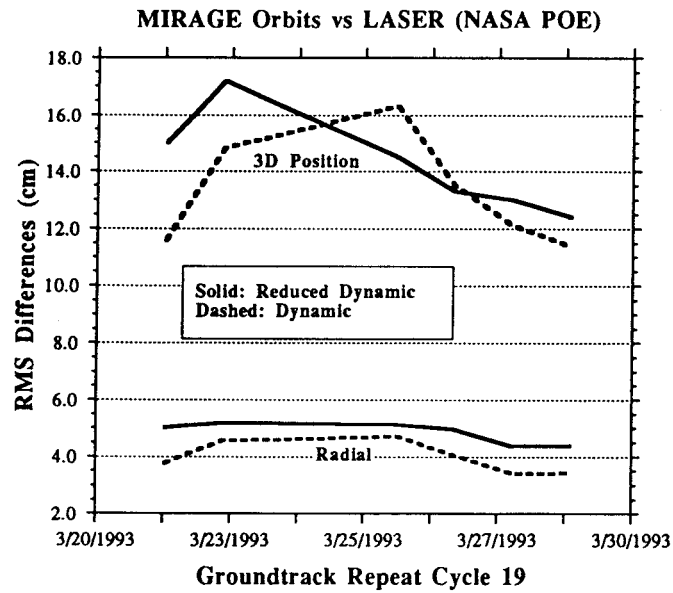
**Figure 3. - MIRAGE Observation Residuals**



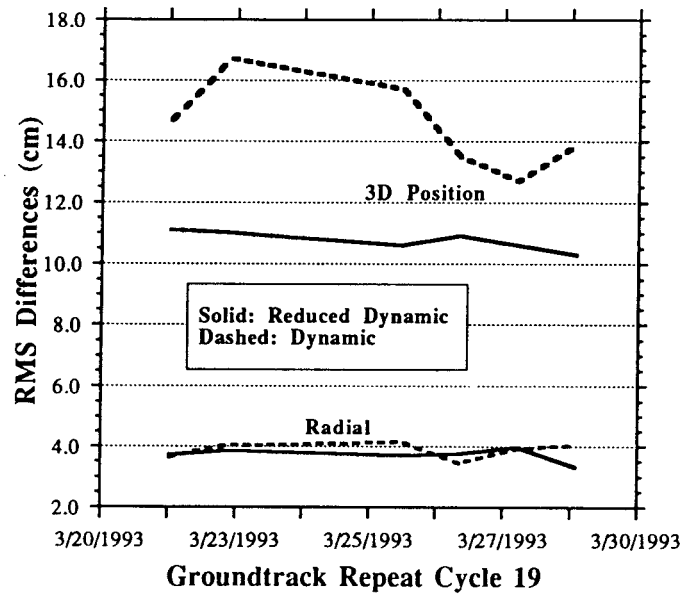
**Figure 4. - MIRAGE GPS Dynamic Orbit Comparisons**



**Figure 5. - MIRAGE Orbit Comparisons**



**MIRAGE Orbits vs GIPSY-OASIS (GPS Reduced Dynamic)**



## **PROCESSING AUTOMATION AND ERROR CHECKING**

One goal of the GDPF was to automate as much of the processing as possible. Beginning with the data collection through the delivery of final products, each aspect of the processing was examined and automated by means of standard Unix scripts and X-Window interfaces to the scripts. Dashed lines in Figure 1. denote automatic procedures that do not require human intervention. User inputs changing from day to day such as the date, duration, and transmitting and receiving participants are controlled via a graphical X-windows interface which eliminates user input errors and ensures operational consistency. Error mail messages are generated to alert operators of malfunctions in the automated non-interactive scripts.

## **OFF-NOMINAL TOPEX/POSEIDON ATTITUDE MODELLING**

Robust processing of off-nominal TOPEX/Poseidon satellite attitude events is available in two ways. First, the actual attitude event change times (e.g., fixed to sinusoidal yaw steering event) are designed as user inputs. Secondly, the trajectory processing can use the attitude quaternions from telemetry. So far, all attitude events, except orbit maintenance maneuvers, have been accurately modelled with the user input overrides. The actual telemetry was only required for the maneuver.

## **LASER AND DORIS DATA TYPES**

In addition to the GPS P-code pseudo-range and carrier phase observables, the MIRAGE software can process Satellite Laser Range (SLR) and Doppler Orbitography and Radiopositioning Integrated by Satellite (DORIS) data. SLR and DORIS data types were incorporated to support TOPEX/Poseidon verification activities. The SLR orbits are used routinely for the Interim Geophysical Data Records (IGDR) science product<sup>8</sup>. Orbit file formats are identical for all data types (i.e., PFILE format); therefore, no interface changes are required for IGDR processing with MIRAGE GPS orbits. A utility has also been developed as part of the MIRAGE software to convert any MIRAGE orbit file into the Precision Orbit Ephemeris (POE) format.

## **TOPEX/POSEIDON MISSION OPERATIONS SUPPORT**

A routine GDPF task is to produce GPSDR almanac predictions for initial acquisition operations. Almanac data are produced twice weekly as a contingency for rapid GPSDR failure recovery. The data are delivered to the Spacecraft Performance Analysis Team for reformatting and subsequent uplink to the GPSDR by the Flight Control Team.

## **GPS ANTI-SPOOFING RESULTS**

During GPS constellation anti-spoofing activities only CA-code pseudo-range and  $L_1$  carrier phase are available from the GPSDR. However, an internal receiver calibration provides for an ionosphere correction to the ground receiver data. Sub-decimeter radial differences have been achieved for limited sets of data by producing an approximate ionosphere calibration. This calibration is derived by subtracting the CA-code carrier phase from the pseudo-range and smoothing the resulting signal to remove multipath. This yields an ionosphere correction that can then be applied to both the CA-code pseudo-range and carrier phase.

## **GDPF RESOURCES**

Required GDPF resources in terms of personnel, computer time and actual time to produce a one day solution are given in Table 5. Members of the operational orbit determination team work on a five day/week schedule. Weekend backlogs are worked off during this schedule. Totals given in Table 5. are for one team member per workstation. For continued operation the GDPF will require a total of three members. The breakdown of tasks for the GDPF team is shown in Table 6. With the automation developed thus far, a single person could easily handle the nominal production. The remainder of the team consists of backups, a lead, and sustaining hardware maintenance personnel.

## **CONCLUSIONS**

Operational orbit determination has been demonstrated for TOPEX/Poseidon using the GPS constellation (~20 satellites), the TOPEX/Poseidon demonstration receiver, six ground station receivers, the GPS Data Handling Facility and the GPS Data Processing Facility. Comparisons between the MIRAGE orbit solutions and other precision orbit solutions based on LASER, DORIS, and GPS yield sub-decimeter radial results. Both the GPS dynamic and reduced dynamic results from MIRAGE appear to exceed the original performance requirements (~one meter radial position) and in fact give results comparable to other geodetic quality software.

**Table 5. - GDPF Processing Performance**

Processing Phase	CPU Time (hr)	Actual Time (hr)
Data Pre-Processing*:		
Collection	0.1	0.1
TOPEX/Poseidon Editing	1.3	1.4
Ground Station Editing	0.4	0.5
Editing	0.1	0.1
Reformatting	<u>0.1</u>	<u>0.1</u>
<b>TOTAL:</b>	<b>2.0</b>	<b>2.2</b>
Orbit Estimation (per iteration):		
Initialization	0.1	0.2
Trajectory Propagation	0.3	0.3
Observation Residual Computation	0.5	0.5
Parameter Estimation	0.1	0.1
Stochastic Parameter Smoothing	<u>0.1</u>	<u>0.1</u>
<b>3 Iteration TOTAL:</b>	<b>3.3</b>	<b>3.6</b>
<b>Archive</b>	<b>0.1</b>	<b>0.2</b>
<b>TOTAL</b>	<b>5.4</b>	<b>6.0</b>

\*Automated processing performed prior to start of work day.

**Table 6. - GDPF Personnel Requirements**

Lead*:	☿
Data Conditioning:	☿
Orbit Determination:	☿
Hardware Maintenance:	♄

\* Lead will also assist and backup data conditioning and orbit determination functions

## ACKNOWLEDGEMENTS

The research described in this paper was carried out by the Jet Propulsion Laboratory, California Institute of Technology, under contract with the National Aeronautics and Space Administration. The authors would like to recognize the technical contributions of Bobby G. Williams to the overall design and development of the MIRAGE software. Also, members of the GDPF team: J. Rodney Jee, Frank Lagattuta, and Ted Drain are appreciated for their effort in producing the results presented in this paper.

## REFERENCES

- 1) Gurtner, W. and G. Mader, "RINEX: The Receiver Independent Exchange Format Version 2," National Geodetic Survey, CSTG GPS Bulletin Vol.3 No.3, September/October 1990.
- 2) Tapley, B.D., "Action items and issues concerning T/P Standards," Center for Space Research, IOM, 25 September 1992.
- 3) McCarthy, D.D., *IERS Standards*, IERS Technical Note 13, Observatoire de Paris, Paris, July 1992.
- 4) GPS Global Site Catalog, GPS Network Operations Group, Jet Propulsion Laboratory, Pasadena, CA., 28 May 1993
- 5) Bertiger, W., and others, "Early Results from the TOPEX/POSEIDON GPS Precise Orbit Determination Demonstration," AAS-93-154, Paper to be presented at the Third Annual AAS/AIAA Spaceflight Mechanics Meeting, Pasadena, CA., 22-24 Feb., 1993.
- 6) Williams, B.G., "Precise Orbit Determination for NASA's Earth observing System Using GPS," *Astrodynamics*, **65**, *Advances in the Astronautical Sciences*, J.K. Soldner, *et al*, eds., Univelt, San Diego, California, 1988, pp. 83-100.
- 7) Wu, S.C., and others, "Reduced-Dynamic Technique for Precise Orbit Determination of Low Earth Satellites," *Astrodynamics*, **65**, *Advances in the Astronautical Sciences*, J.K. Soldner, *et al*, eds., Univelt, San Diego, California, 1988, pp. 101-113
- 8) Williams, B.G., and others, "Short Arc Orbit Determination for Altimeter Calibration and Validation on TOPEX/Poseidon," *Advances in the Astronautical Sciences*, **82**, Univelt, San Diego, California, 1993, pp. 877-888.